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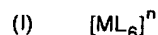
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Harrow, Middlesex HA1 4TY (GB)(54) **Photographic element with light sensitive layer comprising blend of high chloride emulsion grains doped with different metal complexes**

(57) A photographic recording element comprising a support bearing at least one radiation-sensitive silver halide emulsion layer comprising silver halide grains containing greater than 50 mole percent chloride, based on silver, and having greater than 50 percent of their surface area provided by {100} crystal faces, wherein (i) a first fraction which comprises from 10-90 wt% of the silver halide grains consists of grains which have a central portion which contains at least  $10^{-7}$  mole of a hexacoordination metal complex which satisfies formula (I) per mole of silver and less than  $10^{-10}$  mole of a hexacoordination metal complex which satisfies formula (II) per mole of silver, and (ii) a second fraction which comprises from 10-90 wt% of the silver halide grains consists of grains which have a central portion which contains at least  $10^{-10}$  mole of a hexacoordination metal complex which satisfies the formula (II) per mole of silver and less than  $10^{-7}$  mole of a hexacoordination metal complex which satisfies the formula (I) per mole of silver:



wherein n is zero, -1, -2, -3 or -4; M is a filled frontier orbital polyvalent metal ion, other than iridium; and  $L_6$  represents bridging ligands which can be independently selected, provided that at least four of the ligands are anionic ligands, and at least one of the ligands is a cyano ligand or a ligand more electronegative than a cyano ligand;



wherein T is Os or Ru;  $E_4$  represents bridging ligands which can be independently selected;  $E^+$  is E or NZ; r is zero, -1, -2 or -3; and Z is oxygen or sulfur.

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## Description

[0001] This invention is directed to photographic elements comprising a radiation sensitive silver halide emulsion layer useful in photography, including electronic printing methods wherein information is recorded in a pixel-by-pixel mode in a radiation silver halide emulsion layer, where the emulsion layer comprises blended silver halide grains including specified classes of dopants.

[0002] The term "high chloride" in referring to silver halide grains and emulsions indicates that chloride is present in a concentration of greater than 50 mole percent, based on total silver.

[0003] In referring to grains and emulsions containing two or more halides, the halides are named in order of ascending concentrations.

[0004] All references to the periodic table of elements periods and groups in discussing elements are based on the Periodic Table of Elements as adopted by the American Chemical Society and published in the *Chemical and Engineering News*, Feb. 4, 1985, p. 26. The term "Group VIII" is used to generically describe elements in groups 8, 9 and 10.

[0005] The term "cubic grain" is employed to indicate a grain is that bounded by six {100} crystal faces. Typically the corners and edges of the grains show some rounding due to ripening, but no identifiable crystal faces other than the six {100} crystal faces. The six {100} crystal faces form three pairs of parallel {100} crystal faces that are equidistantly spaced.

[0006] The term "cubical grain" is employed to indicate grains that are at least in part bounded by {100} crystal faces satisfying the relative orientation and spacing of cubic grains. That is, three pairs of parallel {100} crystal faces are equidistantly spaced. Cubical grains include both cubic grains and grains that have one or more additional identifiable crystal faces. For example, tetradecahedral grains having six {100} and eight {111} crystal faces are a common form of cubical grains.

[0007] The term "tabular grain" indicates a grain having two parallel major crystal faces (face which are clearly larger than any remaining crystal face) and having an aspect ratio of at least 2.

[0008] The term "aspect ratio" designates the ratio of the equivalent circular diameter of a major face to grain thickness.

[0009] The term "tabular grain emulsion" refers to an emulsion in which tabular grains account for greater than 50 percent of total grain projected area.

[0010] The term "{100} tabular" is employed in referring to tabular grains and tabular grain emulsions in which the tabular grains have {100} major faces.

[0011] The term "central portion" in referring to silver halide grains refers to that portion of the grain structure that is first precipitated accounting for up to 99 percent of total precipitated silver required to form the grains.

[0012] The term "dopant" is employed to indicate any material within the rock salt face centered cubic crystal lattice structure of a silver halide grain other than silver ion or halide ion.

[0013] The term "dopant band" is employed to indicate the portion of the grain formed during the time that dopant was introduced to the grain during precipitation process.

[0014] The term "surface modifier" refers to any material other than silver ion or halide ion that is associated with a portion of the silver halide grains other than the central portion.

[0015] The term "log E" is the logarithm of exposure in lux-seconds.

[0016] Speed is reported as relative log speed, where 1.0 relative log speed units is equal to 0.01 log E.

[0017] The term "contrast" or "γ" is employed to indicate the slope of a line drawn from stated density points on the characteristic curve.

[0018] The term "reciprocity law failure" refers to the variation in response of an emulsion to a fixed light exposure due to variation in the specific exposure time.

[0019] *Research Disclosure* is published by Kenneth Mason Publications, Ltd., Dudley House, 12 North St., Emsworth, Hampshire PO10 7DQ, England.

[0020] In its most commonly practiced form silver halide photography employs a film in a camera to produce, following photographic processing, a negative image on a transparent film support. A positive image for viewing is produced by exposing a photographic print element containing one or more silver halide emulsion layers coated on a reflective white support through the negative image in the camera film, followed by photographic processing. Whereas high bromide silver halide emulsions are the overwhelming commercial choice for camera films, high chloride grain emulsions are the overwhelming commercial choice for photographic print elements. In a relatively recent variation negative image information is retrieved by scanning and stored in digital form. The digital image information is later used to expose imagewise the emulsion layer or layers of the photographic print element. Whether a conventional optical or a digital image printing exposure is employed, it is desired in high chloride emulsions for color paper applications to obtain high photographic speed at the desired sensitometric curve shape.

[0021] A typical example of imaging systems which require that a hard copy be provided from an image which is in digital form is electronic printing of photographic images which involves control of individual pixel exposure. Such a

system provides greater flexibility and the opportunity for improved print quality in comparison to optical methods of photographic printing. In a typical electronic printing method, an original image is first scanned to create a digital representation of the original scene. The data obtained is usually electronically enhanced to achieve desired effects such as increased image sharpness, reduced graininess and color correction. The exposure data is then provided to an electronic printer which reconstructs the data into a photographic print by means of small discrete elements (pixels) that together constitute an image. In a conventional electronic printing method, the recording element is scanned by one or more high energy beams to provide a short duration exposure in a pixel-by-pixel mode using a suitable source, such as a light emitting diode (LED) or laser. A cathode ray tube (CRT) is also sometimes used as a printer light source in some devices. Such methods are described in the patent literature, including, for example, Hioki U.S. Patent 5,126,235; European Patent Application 479 167 A1 and European Patent Application 502 508 A1. Also, many of the basic principles of electronic printing are provided in Hunt, *The Reproduction of Colour*, Fourth Edition, pages 306-307, (1987). Budz et al U.S. Patent 5,451,490 discloses an improved electronic printing method which comprises subjecting a radiation sensitive silver halide emulsion layer of a recording element to actinic radiation of at least  $10^{-4}$  ergs/cm<sup>2</sup> for up to 100  $\mu$  seconds duration in a pixel-by-pixel mode. The radiation sensitive silver halide emulsion layer contains a silver halide grain population comprising at least 50 mole percent chloride, based on silver, forming the grain population projected area. At least 50 percent of the grain population projected area is accounted for by tabular grains that are bounded by {100} major faces having adjacent edge ratios of less than 10, each having an aspect ratio of at least 2. The substitution of a high chloride tabular grain emulsion for a high chloride cubic grain emulsion was demonstrated to reduce high intensity reciprocity failure (HIRF).

**[0022]** Electronic digital printing onto silver halide media frequently is subject to the appearance of various digital printing artifacts. Image artifacts which may be associated with optical scan printing on silver halide media include "digital fringing", "contouring", and "banding". Of the artifacts associated with printing digital images onto silver halide media, "digital fringing", or the formation of visually soft edges, especially around text, probably elicits the greatest objections. This artifact pertains to unwanted density formed in an area of a digital print as a result of a scanning exposure in a different area of the print. Digital fringing may be detected in pixels many lines away from area(s) of higher exposure, creating an underlying minimum density or  $D_{min}$  that reduces sharpness and degrades color reproduction. "Contouring" refers to the formation of discrete density steps in highlight regions where the gradations should appear continuous. Bit limited system modulators (those that use  $\geq 210$  bits, or 1024 DAC levels, designated 10 bit), e.g., may have too few levels to calibrate for density differences that are below the detection threshold of the human eye. A single bit change in exposure may, therefore, produce a density change large enough to see as a step, or contour. "Banding" is the appearance of lines, or bands, having a lower frequency than the individual raster lines, but which are parallel to the line scan direction. The bands arise from non-uniformity in the overlap exposure between scans (e.g., from mechanical vibrations) causing fluctuations in exposure in the overlap areas large enough to produce a visually detectable difference in density.

**[0023]** One of the most important parameters describing suitability of color paper for digital exposure is "dynamic range", which may be defined as the amount of energy that has to be delivered to an emulsion to reach the desired printing density. For most digital printing devices the dynamic range should be equal to 1 logE. Too wide dynamic range may result in the appearance of digital fringing in a color paper. The minimum exposure at which digital fringing becomes visually objectionable varies by digital printing device and emulsion photographic properties. Because fringing increases with exposure, the useful density range for typical commercial color photographic papers printed by scanning laser or LED (light emitting diode) exposures must be restricted to 2.2 or below, less than the full density range of the papers. Fine line images require even lower print densities due to the acute sensitivity of the eye to softening of high contrast edges.

**[0024]** Proper design of the paper's D-log E "characteristic curve" (see, e.g., T. H. James, *The Theory of the Photographic Process*, 4th Ed., Macmillan, 1977, Pp. 501-504) can help minimize the occurrence of digital artifacts. In order to reduce digital fringing, e.g., a relatively high contrast is desired in the shoulder area of the characteristic curve to enable a desired dynamic range. A relatively soft toe is also desired in the characteristic curve, however, to reduce the occurrence of banding and contouring. Lower contrast toe regions of the paper characteristic curves can alleviate contouring in a 10 bit system, e.g., as taught by Kawai, Kokai JP 05/142712-A, but the low contrast also lowers the density threshold for digital fringing.

**[0025]** The use of dopants in silver halide grains to modify photographic performance is well known in the photographic art, as generally illustrated, e.g., by *Research Disclosure*, Item 38957, I. Emulsion grains and their preparation, D. Grain modifying conditions and adjustments, paragraphs (3)-(5). Photographic performance attributes known to be affected by dopants include sensitivity, reciprocity failure, and contrast. The features of high contrast in the shoulder area and relatively soft toe contrast desired for digital printing can be obtained for color paper photographic emulsions through selection of appropriate contrast and speed enhancing dopants.

**[0026]** Using empirical techniques the art has over the years identified many dopants capable of increasing photographic speed. Keevert et al U.S. Patent 4,945,035, e.g., was the first to teach the incorporation of a hexacoordination

complex containing a transition metal and cyano ligands as a dopant in high chloride grains to provide increased sensitivity. Scientific investigations have gradually established that one general class of such speed increasing dopants share the capability of providing shallow electron trapping sites. Olm et al U.S. Patent 5,503,970 and Daubendiek et al U.S. Patents 5,494,789 and 5,503,971, as well as *Research Disclosure*, Vol. 367, Nov. 1994, Item 36736, were the first to set out comprehensive criteria for a dopant to have the capability of providing shallow electron trapping sites.

[0027] The contrast of photographic elements containing silver halide emulsions can generally be increased by incorporating into the silver halide grains a dopant capable of creating deep electron trapping sites, such as illustrated by R. S. Eachus, R. E. Graves and M. T. Olm *J. Chem. Phys.*, Vol. 69, pp. 4580-7 (1978) and *Physica Status Solidi A*, Vol. 57, 429-37 (1980) and R. S. Eachus and M. T. Olm *Annu. Rep. Prog. Chem. Sect. C. Phys. Chem.*, Vol. 83, 3, pp. 3-48 (1986). The use of a hexacoordination complex dopant comprising a transition metal and a nitrosyl or thionitrosyl ligand has been found to be particularly effective at increasing contrast of photographic elements, as disclosed in McDugle et al. U.S. Patent 4,933,272. MacIntyre et al. U.S. Patent 5,597,686 discloses that a combination of an osmium-based transition metal complex containing a nitrosyl or thionitrosyl ligand and a Group 8 transition metal complex containing cyano ligands can result in further improved contrast. U.S. Patents 5,783,373 and 5,783,378 discuss use of combinations of transition metal complex dopants containing a nitrosyl or thionitrosyl ligand with shallow electron trapping dopants (and further with iridium coordination complex dopants for reciprocity performance) for high chloride emulsions in order to provide increased contrast in a photographic print material specifically for use in digital imaging.

[0028] While the use of transition metal complex dopants containing a nitrosyl or thionitrosyl ligand in combination with shallow electron trapping dopants in high chloride emulsions has been found to enable desirable characteristic curve shapes for digital printing of color photographic paper elements, it has been found that combination of such dopants can also result in latent image keeping instability problems. Latent image keeping (LIK) instability refers to a highly undesirable property of changing photographic performance as a function of the time that elapses between exposure and processing. LIK change may be seen as either a loss in speed or density or a gain in speed or density. It would be desirable to provide a photographic element employing a combination of contrast and speed improving dopants in silver halide emulsions with improved latent image keeping performance.

[0029] In one aspect this invention is directed towards a photographic recording element comprising a support bearing at least one radiation-sensitive silver halide emulsion layer comprising silver halide grains containing greater than 50 mole percent chloride, based on silver, and having greater than 50 percent of their surface area provided by {100} crystal faces, wherein

(i) a first fraction which comprises from 10-90 wt% of the silver halide grains, based on total radiation-sensitive silver halide in the layer, consists of grains which have a central portion accounting for up to 99 percent of total silver which contains at least  $10^{-7}$  mole of a hexacoordination metal complex which satisfies formula (I) per mole of silver and less than  $10^{-10}$  mole of a hexacoordination metal complex which satisfies formula (II) per mole of silver, and

(ii) a second fraction which comprises from 10-90 wt% of the silver halide grains, based on total radiation-sensitive silver halide in the layer, consists of grains which have a central portion accounting for up to 99 percent of total silver which contains at least  $10^{-10}$  mole of a hexacoordination metal complex which satisfies the formula (II) per mole of silver and less than  $10^{-7}$  mole of a hexacoordination metal complex which satisfies the formula (I) per mole of silver:



wherein n is zero, -1, -2, -3 or -4,

M is a filled frontier orbital polyvalent metal ion, other than iridium, and

$L_6$  represents bridging ligands which can be independently selected, provided that at least four of the ligands are anionic ligands, and at least one of the ligands is a cyano ligand or a ligand more electronegative than a cyano ligand;



wherein T is Os or Ru;

$E_4$  represents bridging ligands which can be independently selected;

$E'$  is E or NZ;

r is zero, -1, -2 or -3; and

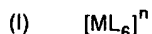
Z is oxygen or sulfur.

[0030] In another aspect, this invention is directed to an electronic printing method which comprises subjecting a radiation sensitive silver halide emulsion layer of a recording element to actinic radiation of at least  $10^{-4}$  ergs/cm<sup>2</sup> for up to 100  $\mu$  seconds duration in a pixel-by-pixel mode, wherein the silver halide emulsion layer is comprised of first and second fractions of silver halide grains as described above.

[0031] It has been discovered that significantly improved latent image keeping performance can be obtained for optical and digital exposed elements which comprise a blend of separate fractions of silver halide grains in an emulsion layer, each of which fraction is differentially doped with a dopant of Formula (I) and a dopant of Formula (II) as described above, while substantially maintaining desired relatively soft toe and dynamic range parameters. In a preferred practical application, the advantages of the invention can be transformed into increased throughput of digital artifact-free color print images while exposing each pixel sequentially in synchronism with the digital data from an image processor.

[0032] In one embodiment, the present invention represents an improvement on the electronic printing method disclosed by Budz et al, cited above. Specifically, this invention in one embodiment is directed to an electronic printing method which comprises subjecting a radiation sensitive silver halide emulsion layer of a recording element to actinic radiation of at least  $10^{-4}$  ergs/cm<sup>2</sup> for up to 100  $\mu$  seconds duration in a pixel-by-pixel mode. The present invention realizes an improvement in latent image keeping by modifying the radiation sensitive silver halide emulsion layer. While certain embodiments of the invention are specifically directed towards electronic printing, use of the elements of the invention is not limited to such specific embodiment, and it is specifically contemplated that the elements of the invention are also well suited for conventional optical printing.

[0033] In accordance with the invention, a first fraction of the silver halide grains in an emulsion layer contain a shallow electron trapping hexacoordination complex dopant satisfying the formula:

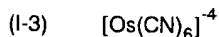
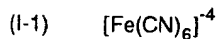


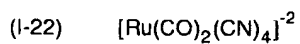
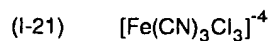
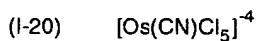
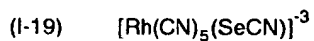
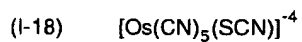
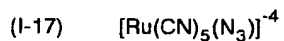
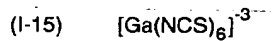
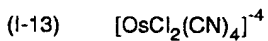
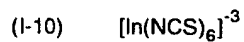
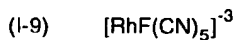
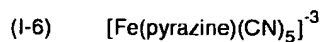
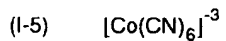
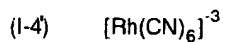
where n is zero, -1, -2, -3 or -4; M is a filled frontier orbital polyvalent metal ion, other than iridium, preferably Fe<sup>+2</sup>, Ru<sup>+2</sup>, Os<sup>+2</sup>, Co<sup>+3</sup>, Rh<sup>+3</sup>, Pd<sup>+4</sup> or Pt<sup>+4</sup>, more preferably an iron, ruthenium or osmium ion, and most preferably a ruthenium ion; and L<sub>6</sub> represents six bridging ligands which can be independently selected, provided that least four of the ligands are anionic ligands and at least one (preferably at least 3 and optimally at least 4) of the ligands is a cyano ligand or a ligand more electronegative than a cyano ligand. Any remaining ligands can be selected from among various other bridging ligands, including aquo ligands, halide ligands (specifically, fluoride, chloride, bromide and iodide), cyanate ligands, thiocyanate ligands, selenocyanate ligands, tellurocyanate ligands, and azide ligands. Hexacoordinated transition metal complexes of Formula (I) which include six cyano ligands are specifically preferred.

[0034] Illustrations of specifically contemplated Formula (I) hexacoordination complexes for inclusion in the high chloride grains are provided by Bell U.S. Patents 5,474,888, 5,470,771 and 5,500,335, Olm et al U.S. Patent 5,503,970 and Daubendiek et al U.S. Patents 5,494,789 and 5,503,971, and Keevert et al U.S. Patent 4,945,035, as well as Murakami et al Japanese Patent Application Hei-2[1990]-249588, and *Research Disclosure* Item 36736. Useful neutral and anionic organic ligands for dopant hexacoordination complexes are disclosed by Olm et al U.S. Patent 5,360,712 and Kuromoto et al U.S. Patent 5,462,849.

[0035] Dopant of Formula (I) is preferably introduced into the first fraction of high chloride grains after at least 50 (most preferably 75 and optimally 80) percent of the silver has been precipitated for such grains, but before precipitation of the central portion of the grains has been completed. Preferably dopant of Formula (I) is introduced before 98 (most preferably 95 and optimally 90) percent of the silver has been precipitated. Stated in terms of the fully precipitated grain structure, the Formula (I) dopant is preferably present in an interior shell region that surrounds at least 50 (most preferably 75 and optimally 80) percent of the silver and, with the more centrally located silver, accounts the entire central portion (99 percent of the silver), most preferably accounts for 95 percent, and optimally accounts for 90 percent of the silver halide forming the high chloride grains. The Formula (I) dopant can be distributed throughout the interior shell region delimited above or can be added as one or more bands within the interior shell region.

[0036] The following are specific illustrations of Formula (I) dopants:





[0037] When the Formula (I) dopants have a net negative charge, it is appreciated that they are associated with a

counter ion when added to the reaction vessel during precipitation. The counter ion is of little importance, since it is ionically dissociated from the dopant in solution and is not incorporated within the grain. Common counter ions known to be fully compatible with silver chloride precipitation, such as ammonium and alkali metal ions, are contemplated. It is noted that the same comments apply to Formula (II) dopants, otherwise described below.

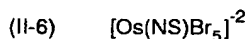
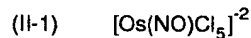
**[0038]** Further in accordance with the invention, a second fraction of the silver halide grains contain a contrast increasing hexacoordination complex dopant satisfying the formula (II), which second fraction of grains is in the same emulsion layer which contains the first fraction of grains doped with a Formula (I) dopant. Coordination complexes of Formula (II) are represented by the formula:



wherein T is Os or Ru; E is a bridging ligand; E' is E or NZ; r is zero, -1, -2 or -3; and Z is oxygen or sulfur. The E ligands can take the form of any independently selected remaining bridging ligands, including aquo ligands, halide ligands (specifically, fluoride, chloride, bromide and iodide), cyano ligand, cyanate ligands, thiocyanate ligands, selenocyanate ligands, tellurocyanate ligands, and azide ligands. Cyano and halide ligands are generally preferred, and hexacoordinated transition metal complexes of Formula (II) which include 5 halide or cyano ligands are specifically preferred. Suitable coordination complexes satisfying the above formula are found in McDugle et al U.S. Patent 4,933,272.

**[0039]** Dopant of Formula (II) may be introduced anywhere within the central portion of the high chloride silver halide grains of the second fraction, but is preferably introduced into the second fraction of grains from 10 to 75 percent of the silver halide forming the high chloride grains. The Formula (II) dopant can be distributed throughout the central portion or can be added as one or more bands within the central portion region.

**[0040]** The following are specific illustrations of Formula (II) compounds:



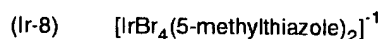
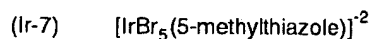
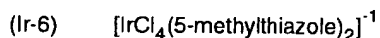
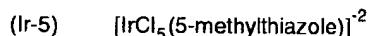
The most preferred nitrosyl ligand containing osmium-based transition metal complex is  $[Os(NO)Cl_5]^{-2}$ , which prior to its incorporation into a silver halide grain is associated with a cation, typically  $2Cs^{+1}$ .

**[0041]** In accordance with the invention, a first fraction of the silver halide grains in a light sensitive photographic element consists of grains which have a central portion accounting for up to 99 percent of total silver which contains at least  $10^{-7}$  mole (preferably from  $10^{-7}$  to  $10^{-3}$  mole, and more preferably from  $10^{-6}$  to  $10^{-4}$  mole) of a hexacoordination metal complex which satisfies formula (I) per mole of silver and less than  $10^{-10}$  mole (more preferably less than  $10^{-11}$  mole) of a hexacoordination metal complex which satisfies formula (II) per mole of silver, which first fraction comprises from 10-90 wt% of the silver halide grains, preferably 25-75 wt% and more preferably 40-60 wt%, based on total radiation-sensitive silver halide in the layer. A second fraction of the silver halide grains in the light sensitive layer consists of grains which have a central portion accounting for up to 99 percent of total silver which contains at least  $10^{-10}$  mole (preferably from  $10^{-10}$  to  $10^{-7}$  mole, and more preferably from  $10^{-9}$  to  $10^{-8}$  mole) of a hexacoordination metal complex which satisfies the formula (II) per mole of silver and less than  $10^{-7}$  mole (more preferably less than  $10^{-8}$  mole)

of a hexacoordination metal complex which satisfies the formula (I) per mole of silver, which second fraction comprises from 10-90 wt% of the silver halide grains, preferably 25-75 wt% and more preferably 40-60 wt%, based on total radiation-sensitive silver halide in the layer.

[0042] The silver halide grains of each of the first and second fractions contained in an emulsion layer of a photographic element in accordance with the invention may also include other dopants. Doping with iridium hexachloride complexes, e.g., is commonly performed to reduce reciprocity law failure in silver halide emulsions. According to the photographic law of reciprocity, a photographic element should produce the same image with the same exposure, even though exposure intensity and time are varied. For example, an exposure for 1 second at a selected intensity should produce exactly the same result as an exposure of 2 seconds at half the selected intensity. When photographic performance is noted to diverge from the reciprocity law, this is known as reciprocity failure. Specific iridium dopants include those illustrated in high chloride emulsions by Bell U.S. Patents 5,474,888, 5,470,771 and 5,500,335 and McIntyre et al 5,597,686. Specific combinations of iridium and other metal dopants may additionally be found in U.S. Patents 4,828,962, 5,153,110, 5,219,722, 5,227,286, and 5,229,263, and European Patent Applications EP 0 244 184, EP 0 405 938, EP 0 476 602, EP 0 488 601, EP 0 488 737, EP 0 513 748, and EP 0 514 675. In accordance with particularly preferred embodiments, an iridium coordination complex containing at least one thiazole or substituted thiazole ligand may be employed. The thiazole ligands may be substituted with any photographically acceptable substituent which does not prevent incorporation of the dopant into the silver halide grain. Exemplary substituents include lower alkyl (e.g., alkyl groups containing 1-4 carbon atoms), and specifically methyl. A specific example of a substituted thiazole ligand which may be used in accordance with the invention is 5-methylthiazole. The iridium dopant preferably is a hexacoordination complex having ligands each of which are more electropositive than a cyano ligand. In a specifically preferred form the remaining non-thiazole or non-substituted-thiazole ligands of the iridium coordination complex dopants are halide ligands.

[0043] Iridium dopant is preferably introduced into the high chloride grains of each of the first and second portions after at least 50 (most preferably 85 and optimally 90) percent of the silver has been precipitated, but before precipitation of the central portion of the grains has been completed. Preferably iridium dopant is introduced before 99 (most preferably 97 and optimally 95) percent of the silver has been precipitated. Stated in terms of the fully precipitated grain structure, iridium dopant is preferably present in an interior shell region that surrounds at least 50 (most preferably 85 and optimally 90) percent of the silver and, with the more centrally located silver, accounts the entire central portion (99 percent of the silver), most preferably accounts for 97 percent, and optimally accounts for 95 percent of the silver halide forming the high chloride grains. The iridium dopant can be distributed throughout the interior shell region delimited above or can be added as one or more bands within the interior shell region. Iridium dopant can be employed in any conventional useful concentration. A preferred concentration range is from  $10^{-9}$  to  $10^{-4}$  mole per silver mole. Iridium is most preferably employed in a concentration range of from  $10^{-8}$  to  $10^{-5}$  mole per silver mole. Specific illustrations of iridium dopants include the following:





[0044] As with dopants of Formula (I) and (II), when iridium dopants have a net negative charge, it is appreciated that they are associated with a counter ion when added to the reaction vessel during precipitation. Common counter ions known to be fully compatible with silver chloride precipitation, such as ammonium and alkali metal ions, are contemplated.

[0045] Emulsions demonstrating the advantages of the invention can be realized by modifying the precipitation of conventional high chloride silver halide grains having predominantly (>50%) {100} crystal faces to obtain separate fractions of grains incorporating the dopants of Formula (I) and Formula (II) as described above, and subsequently blending the two fractions of grains into a single emulsion layer. The performance improvement described in accordance with the invention may be obtained for silver halide grains employing conventional gelatino-peptizer, as well as oxidized gelatin (e.g., gelatin having less than 30 micromoles of methionine per gram). Accordingly, in specific embodiments of the invention, it is specifically contemplated to use significant levels (i.e., greater than 1 weight percent of total peptizer) of conventional gelatin (e.g., gelatin having at least 30 micromoles of methionine per gram) as a gelatino-peptizer for the silver halide grains of the emulsions of the invention. In preferred embodiments of the invention, gelatino-peptizer is employed which comprises at least 50 weight percent of gelatin containing at least 30 micromoles of methionine per gram, as it is frequently desirable to limit the level of oxidized low methionine gelatin which may be used for cost and certain performance reasons.

[0046] The silver halide grains precipitated contain greater than 50 mole percent chloride, based on silver. Preferably the grains contain at least 70 mole percent chloride and, optimally at least 90 mole percent chloride, based on silver. Iodide can be present in the grains up to its solubility limit, which is in silver iodochloride grains, under typical conditions of precipitation, 11 mole percent, based on silver. It is preferred for most photographic applications to limit iodide to less than 5 mole percent iodide, most preferably less than 2 mole percent iodide, based on silver.

[0047] Silver bromide and silver chloride are miscible in all proportions. Hence, any portion, up to 50 mole percent, of the total halide not accounted for chloride and iodide, can be bromide. For color reflection print (i.e., color paper) uses bromide is typically limited to less than 10 mole percent based on silver and iodide is limited to less than 1 mole percent based on silver.

[0048] In a widely used form high chloride grains are precipitated to form cubic grains, that is, grains having {100} major faces and edges of equal length. In practice ripening effects usually round the edges and corners of the grains to some extent. However, except under extreme ripening conditions substantially more than 50 percent of total grain surface area is accounted for by {100} crystal faces.

[0049] High chloride tetradecahedral grains are a common variant of cubic grains. These grains contain 6 {100} crystal faces and 8 {111} crystal faces. Tetradecahedral grains are within the contemplation of this invention to the extent that greater than 50 percent of total surface area is accounted for by {100} crystal faces.

[0050] Although it is common practice to avoid or minimize the incorporation of iodide into high chloride grains employed in color paper, it has been recently observed that silver iodochloride grains with {100} crystal faces and, in some instances, one or more {111} faces offer exceptional levels of photographic speed. In these emulsions iodide is incorporated in overall concentrations of from 0.05 to 3.0 mole percent, based on silver, with the grains having a surface shell of greater than 50 Å that is substantially free of iodide and a interior shell having a maximum iodide concentration that surrounds a core accounting for at least 50 percent of total silver. Such grain structures are illustrated by Chen et al EPO 0 718 679.

[0051] In another improved form the high chloride grains can take the form of tabular grains having {100} major faces. Preferred high chloride {100} tabular grain emulsions are those in which the tabular grains account for at least 70 (most preferably at least 90) percent of total grain projected area. Preferred high chloride {100} tabular grain emulsions have average aspect ratios of at least 5 (most preferably at least >8). Tabular grains typically have thicknesses of less than 0.3 µm, preferably less than 0.2 µm, and optimally less than 0.07 µm. High chloride {100} tabular grain emulsions and their preparation are disclosed by Maskasky U.S. Patents 5,264,337 and 5,292,632, House et al U.S. Patent 5,320,938, Brust et al U.S. Patent 5,314,798 and Chang et al U.S. Patent 5,413,904.

[0052] Once high chloride grains having predominantly {100} crystal faces have been precipitated to form two grain fractions differentially doped with dopants of Formula (I) and Formula (II) described above, chemical and spectral sensitization, followed by the addition of conventional addenda to adapt the emulsion for the imaging application of choice can take any convenient conventional form. The separately precipitated grain fractions may be individually chemically and spectrally sensitized before being blended together, or may be first blended and then sensitized. Conventional features are further illustrated by *Research Disclosure*, Item 38957, cited above, particularly:

- III. Emulsion washing;
- IV. Chemical sensitization;
- V. Spectral sensitization and desensitization;
- VII. Antifoggants and stabilizers;
- VIII. Absorbing and scattering materials;

IX. Coating and physical property modifying addenda; and

X. Dye image formers and modifiers."

**[0053]** As pointed out by Bell, cited above, some additional silver halide, typically less than 1 percent, based on total silver, can be introduced to facilitate chemical sensitization. It is also recognized that silver halide can be epitaxially deposited at selected sites on a host grain to increase its sensitivity. For example, high chloride {100} tabular grains with corner epitaxy are illustrated by Maskasky 5,275,930. For the purpose of providing a clear demarcation, the term "silver halide grain" is herein employed to include the silver necessary to form the grain up to the point that the final {100} crystal faces of the grain are formed. Silver halide later deposited that does not overlie the {100} crystal faces previously formed accounting for at least 50 percent of the grain surface area is excluded in determining total silver forming the silver halide grains. Thus, the silver forming selected site epitaxy is not part of the silver halide grains while silver halide that deposits and provides the final {100} crystal faces of the grains is included in the total silver forming the grains, even when it differs significantly in composition from the previously precipitated silver halide.

**[0054]** In the simplest contemplated form a photographic element of the invention can consist of a single emulsion layer satisfying the emulsion description provided above coated on a conventional photographic support, such as those described in *Research Disclosure*, Item 38957, cited above, XVI. Supports. In one preferred form the support is a white reflective support, such as photographic paper support or a film support that contains or bears a coating of a reflective pigment. To permit a print image to be viewed using an illuminant placed behind the support, it is preferred to employ a white translucent support, such as a Duratrans™ or Duraclear™ support.

**[0055]** The photographic elements and printing methods of the invention can be used to form either silver or dye images in the recording element. In a simple form a single radiation sensitive emulsion layer unit is coated on the support. The elements can contain one or more high chloride silver halide emulsions satisfying the requirements of the invention. When a dye imaging forming compound, such as a dye-forming coupler, is present it can be in an emulsion layer or in a layer coated in contact with the emulsion layer. With a single emulsion layer unit a monochromatic image is obtained.

**[0056]** In a preferred embodiment the invention employs recording elements which are constructed to contain at least three silver halide emulsion layer units. A suitable multicolor, multilayer format for a recording element used in the invention is represented by Structure I.

Blue-sensitized
yellow dye image-forming silver halide emulsion unit
Interlayer
Green-sensitized
magenta dye image-forming silver halide emulsion unit
Interlayer
Red-sensitized
cyan dye image-forming silver halide emulsion unit
//// Support ////

STRUCTURE I

wherein the red-sensitized, cyan dye image-forming silver halide emulsion unit is situated nearest the support; next in order is the green-sensitized, magenta dye image-forming unit, followed by the uppermost blue-sensitized, yellow dye image-forming unit. The image-forming units are separated from each other by hydrophilic colloid interlayers containing an oxidized developing agent scavenger to prevent color contamination. Silver halide emulsions satisfying the requirements described above can be present in any one or combination of the emulsion layer units. Additional useful multicolor, multilayer formats for an element of the invention include Structures II-IV as described in U.S. Patent 5,783,373 referenced above. Each of such structures in accordance with the invention would contain at least one blended silver

halide emulsion comprised of high chloride grains having at least 50 percent of their surface area bounded by {100} crystal faces and containing first and second fractions of grains containing dopants of Formula (I) and Formula (II) as described above. Preferably each of the emulsion layer units contain an emulsion satisfying these criteria.

[0057] Conventional features that can be incorporated into multilayer (and particularly multicolor) recording elements contemplated for use in the invention are illustrated by *Research Disclosure*, Item 38957, cited above:

- XI. Layers and layer arrangements
- XII. Features applicable only to color negative
- XIII. Features applicable only to color positive

- B. Color reversal
- C. Color positives derived from color negatives

#### XIV. Scan facilitating features.

[0058] The recording elements comprising the radiation sensitive high chloride emulsion layers according to this invention can be conventionally optically printed, or in accordance with a particular embodiment of the invention can be image-wise exposed in a pixel-by-pixel mode using suitable high energy radiation sources typically employed in electronic printing methods. Suitable actinic forms of energy encompass the ultraviolet, visible and infrared regions of the electromagnetic spectrum as well as electron-beam radiation and is conveniently supplied by beams from one or more light emitting diodes or lasers, including gaseous or solid state lasers. Exposures can be monochromatic, orthochromatic or panchromatic. For example, when the recording element is a multilayer multicolor element, exposure can be provided by laser or light emitting diode beams of appropriate spectral radiation, for example, infrared, red, green or blue wavelengths, to which such element is sensitive. Multicolor elements can be employed which produce cyan, magenta and yellow dyes as a function of exposure in separate portions of the electromagnetic spectrum, including at least two portions of the infrared region, as disclosed in the previously mentioned U.S. Patent No. 4,619,892. Suitable exposures include those up to 2000 nm, preferably up to 1500 nm. The exposing source need, of course, provide radiation in only one spectral region if the recording element is a monochrome element sensitive to only that region (color) of the electromagnetic spectrum. Suitable light emitting diodes and commercially available laser sources are described in the examples. Imagewise exposures at ambient, elevated or reduced temperatures and/or pressures can be employed within the useful response range of the recording element determined by conventional sensitometric techniques, as illustrated by T.H. James, *The Theory of the Photographic Process*, 4th Ed., Macmillan, 1977, Chapters 4, 6, 17, 18 and 23.

[0059] The quantity or level of high energy actinic radiation provided to the recording medium by the exposure source is generally at least  $10^{-4}$  ergs/cm<sup>2</sup>, typically in the range of  $10^{-4}$  ergs/cm<sup>2</sup> to  $10^{-3}$  ergs/cm<sup>2</sup> and often from  $10^{-3}$  ergs/cm<sup>2</sup> to  $10^2$  ergs/cm<sup>2</sup>. Exposure of the recording element in a pixel-by-pixel mode as known in the prior art persists for only a very short duration or time. Typical maximum exposure times are up to 100  $\mu$  seconds, often up to 10  $\mu$  seconds, and frequently up to only 0.5  $\mu$  seconds. Single or multiple exposures of each pixel are contemplated. The pixel density is subject to wide variation, as is obvious to those skilled in the art. The higher the pixel density, the sharper the images can be, but at the expense of equipment complexity. In general, pixel densities used in conventional electronic printing methods of the type described herein do not exceed  $10^7$  pixels/cm<sup>2</sup> and are typically in the range of  $10^4$  to  $10^6$  pixels/cm<sup>2</sup>. An assessment of the technology of high-quality, continuous-tone, color electronic printing using silver halide photographic paper which discusses various features and components of the system, including exposure source, exposure time, exposure level and pixel density and other recording element characteristics is provided in Firth et al., *A Continuous-Tone Laser Color Printer*, Journal of Imaging Technology, Vol. 14, No. 3, June 1988. As previously indicated herein, a description of some of the details of conventional electronic printing methods comprising scanning a recording element with high energy beams such as light emitting diodes or laser beams, are set forth in Hioki U.S. Patent 5,126,235, European Patent Applications 479 167 A1 and 502 508 A1.

[0060] Once imagewise exposed, the recording elements can be processed in any convenient conventional manner to obtain a viewable image. As demonstrated in the examples below, photographic elements in accordance with the invention demonstrate improved latent image keeping performance, decreasing the impact of delays in processing which may occur after imagewise exposure. Conventional processing is illustrated, e.g., by *Research Disclosure*, Item 38957, cited above:

- XVIII. Chemical development systems
- XIX. Development
- XX. Desilvering, washing, rinsing and stabilizing

## Examples

[0061] This invention can be better appreciated by reference to the following Examples. Emulsions EM-1 through EM-3 and A through R illustrate the preparation of radiation sensitive high chloride emulsions, both for comparison and inventive emulsions. Examples 1 and 2 illustrate that recording elements containing layers of emulsions in accordance with the invention exhibit characteristics that make them particularly useful in very fast optical printers and in electronic printing methods of the type described herein.

## EMULSION PRECIPITATIONS

[0062] Emulsion EM-1: A reaction vessel contained 6.92 L of a solution that was 3.8% in regular gelatin and contained 1.71 g of a Pluronic antifoam agent. To this stirred solution at 46°C 83.5 mL of 3.0 M NaCl was dumped, and soon after 28.3 mL of dithiooctanediol solution was poured into the reactor. A half minute after addition of dithiooctanediol solution, 104.5 mL of a 2.8 M AgNO<sub>3</sub> solution and 107.5 mL of 3.0 M NaCl were added simultaneously at 209 mL/min for 0.5 minute. The vAg set point was chosen equal to that observed in the reactor at this time. Then the 2.8 M silver nitrate solution and the 3.0 M sodium chloride solution were added simultaneously with a constant flow at 209 mL/min over 20.75 minutes. During precipitation, 33.08 milligrams per silver mole of Formula (I) dopant K<sub>4</sub>Ru(CN)<sub>6</sub> was added during 75 to 80% of grain formation, and 2.20 milligrams per silver mole of K<sub>2</sub>IrCl<sub>5</sub> (5-Methyl-Thiazole)2H<sub>2</sub>O was added during 90 to 95% of grain formation. The resulting silver chloride emulsion had a cubic shape that was 0.38 μm in edgelenh. The emulsion was then washed using an ultrafiltration unit, and its final pH and pCl were adjusted to 5.6 and 1.8, respectively.

Emulsion EM-2: This emulsion was precipitated exactly as Emulsion EM-1, except that Formula (I) dopant K<sub>4</sub>Ru(CN)<sub>6</sub> was not added during precipitation, and that 3.0 micrograms per silver mole of Formula (II) dopant cesium pentachloronitrosylosmate (Cs<sub>2</sub>(II)Os[NO]Cl<sub>5</sub>) was added during precipitation during 5 to 70% of grain formation.

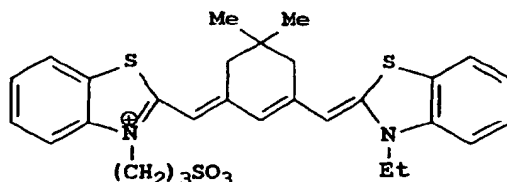
Emulsion EM-3: This emulsion was precipitated exactly as Emulsion EM-1, except that 1.50 micrograms per silver mole of Formula (II) dopant cesium pentachloronitrosylosmate (Cs<sub>2</sub>(II)Os[NO]Cl<sub>5</sub>) was additionally added during precipitation during 5 to 70% of grain formation, and Formula (I) dopant K<sub>4</sub>Ru(CN)<sub>6</sub> was added during 75 to 80% of grain formation at 16.54 milligrams per silver mole.

## SENSITIZATION OF EMULSIONS

[0063] The emulsions were each optimally sensitized by the customary techniques using two basic sensitization schemes. The sequence of chemical sensitizers, spectral sensitizers, and antifoggants addition are the same for each finished emulsion. Both colloidal gold sulfide or gold(I) (as disclosed in U.S. Pat. No. 5, 945,270) and hypo (Na<sub>2</sub>S<sub>2</sub>O<sub>3</sub>) were used for chemical sensitization. Detailed procedures are described in the Examples below.

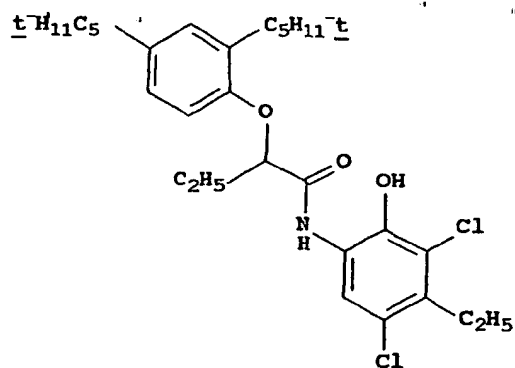
[0064] In red-sensitized emulsions the following red spectral sensitizing dye was used:

Spectral Sensitizing Dye A:



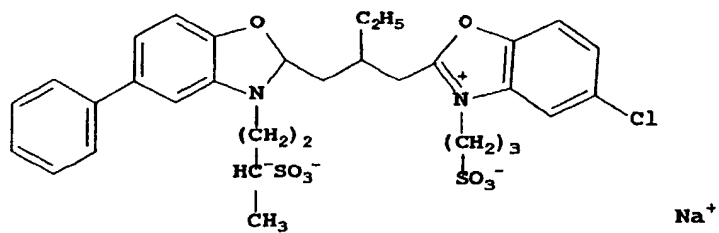
[0065] Just prior to coating on resin coated paper support red-sensitized emulsions were dual-mixed with cyan dye forming coupler A:

## Coupler A:



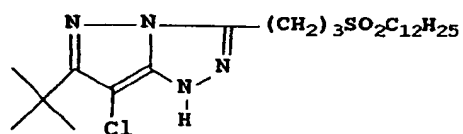
[0066] In green-sensitized emulsions the following green spectral sensitizing dye was used:

## Spectral Sensitizing Dye B:



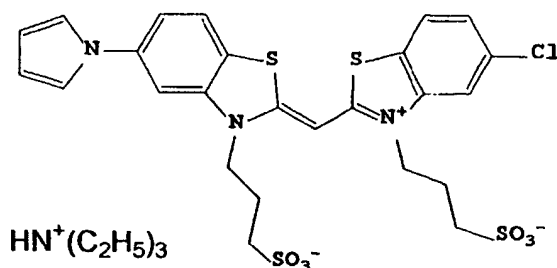
[0067] Just prior to coating on resin coated paper support green-sensitized emulsions were dual-mixed with magenta dye forming coupler B:

## Coupler B:



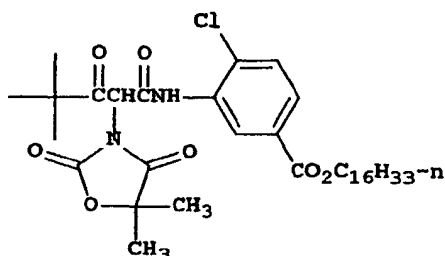
[0068] In blue-sensitized emulsions the following blue spectral sensitizing dye was used:

## Spectral Sensitizing Dye C:



**[0069]** Just prior to coating on resin coated paper support blue-sensitized emulsions were dual-mixed with yellow dye forming coupler C:

## Coupler C:



**[0070]** The red-sensitized emulsions were coated at 194 mg silver per square meter, green-sensitized emulsions were coated at 108 mg silver per square meter, and blue-sensitized emulsions were coated at 280 mg silver per square meter on resin-coated paper support. The coatings were overcoated with gelatin layer and the entire coating was hardener with bis(vinylsulfonmethyl)ether.

## PHOTOGRAPHIC COMPARISONS

**[0071]** Coatings were exposed through a step wedge with 3000 K tungsten source at 0.1 second for red and green sensitized emulsions. Speed is reported as relative log speed at specified level above the minimum density as presented in the following Examples. In relative log speed units a speed difference of 30, for example, is a difference of 0.30 log E, where E is exposure in lux-seconds. These exposures will be referred to as "Optical Sensitivity" in the following Examples.

**[0072]** Coatings were also exposed with 3 color laser sensitometric exposure apparatus at 691 nm (red sensitized emulsions), 532 nm (green sensitized emulsions) or 470 nm (blue sensitized emulsions), a resolution of 98.4 pixels/cm, a pixel pitch of 100  $\mu$ m, and the exposure time of 1 microsecond per pixel. These exposures will be referred to as "Digital Sensitivity" in the following Examples.

**[0073]** All coatings were processed in Kodak™ Ektacolor RA-4. Relative optical and laser SPEED values were reported at density level equal to 0.80, TOE values were reported as the density at 0.80 density level minus 0.3 logE, and INmax values were reported as the density measured 1.0 logE from the threshold speed that is measured at the density equal to Dmin + 0.04. INmax provides an estimate of the "dynamic range" of the photographic element. The higher the INmax, the narrower the dynamic range, and the less sensitive is a photographic element for fringing. To provide a measurement of Latent Image Keeping performance, processing for samples of each of the optical and laser exposed coatings was delayed (2 and 24 hours vs. 5 minutes for the optical exposures; and 2 minutes and 2 and 24 hours vs. 20 seconds for the laser exposures).

## EXAMPLE 1

[0074] This example compares effects of blending of emulsion doped with Formula (I) dopant  $K_4Ru(CN)_6$  with emulsion doped with Formula (II) dopant  $Cs_2(II)Os[NO]Cl_5$  on optical and laser Latent Image Keeping (LIK). In each case, silver chloride cubic emulsions sensitized for red color record were used. The sensitization details are as follows:

Emulsion A: A portion of silver chloride Emulsion EM-1 was optimally sensitized by the addition of p-glutamido-phenyl disulfide (GDPD) followed by addition of the optimum amount of hypo followed by addition of gold(I). The emulsion was then heated to 65°C and held at this temperature for 30 minutes with subsequent addition of 1-(3-acetamidophenyl)-5-mercaptopotrazole followed by addition of potassium hexachloroiridate and followed by bromide addition. Then the emulsion was cooled to 40°C and Spectral Sensitizing dye A was added. The thus obtained silver chloride emulsion was designated as emulsion A.

Emulsion B: A portion of silver chloride Emulsion EM-2 was sensitized exactly as in the procedure for the preparation of emulsion A. The thus obtained silver chloride emulsion was designated as emulsion B.

Emulsion C: A portion of silver chloride Emulsion EM-3 was sensitized exactly as in the procedure for the preparation of emulsion A. The thus obtained silver chloride emulsion was designated as emulsion C.

Emulsion D: A equal portion of silver chloride Emulsion EM-1 and EM-2 was blended and then sensitized exactly as in the procedure for the preparation of emulsion A. The thus obtained silver chloride emulsion was designated as emulsion D. The "total" amounts of each dopant per Ag mole are the same as in Emulsion C.

Emulsion E: A equal portion of silver chloride Emulsion A and B was blended. The thus obtained silver chloride emulsion was designated as emulsion E. The "total" amounts of each dopant per Ag mole are the same as in Emulsion C.

Sensitometric data and LIK responses is summarized in Table I and Table II.

Table I.

Optical Sensitometry and Optical LIK Data.								
Emulsion	Dmin	SPEED	TOE	INmax	Optical LIK			
					5 min to 2 hr		5 min to 24 hr	
					$\Delta D$ at SPEED	$\Delta D$ at SPEED+ 0.2logE	$\Delta D$ at SPEED	$\Delta D$ at SPEED+ 0.2logE
A	0.098	160	0.408	1.712	0.0667	0.1083	0.0543	0.1042
B	0.099	143	0.334	1.986	0.0499	0.0667	0.0374	0.0541
C	0.098	153	0.332	2.124	0.0625	0.1012	0.1251	0.2334
D	0.101	153	0.389	2.086	-	-	-	-
E	0.098	155	0.397	2.104	0	0.0083	0.0124	0.0167

Table II

Laser Sensitometry and Laser LK Data.									
Emulsion	Dmin	SPEED	TOE	INmax	Laser LK				
					20 sec to 2 min		20 sec to 2 hr		
					$\Delta D$ at SPEED	$\Delta D$ at SPEED + $0.2 \log E$	$\Delta D$ at SPEED	$\Delta D$ at SPEED + $0.2 \log E$	$\Delta D$ at SPEED + $0.2 \log E$
A	0.101	141	0.397	1.551	0.0069	0.0185	0.0392	0.0585	0.1149
B	0.099	122	0.331	1.936	0.0071	0.0074	0.0221	0.0428	0.0392
C	0.101	133	0.321	2.372	0.0101	0.0429	0.0929	0.1572	0.3025
D	0.097	133	0.382	2.202	0.0061	0.0084	0.0391	0.0571	0.0821
E	0.098	135	0.389	2.184	0.0092	0.0092	0.0328	0.0574	0.0643



[0075] It is clear from the Tables I and II, that sensitization of a blended emulsion (Emulsion D) produce about the same photographic response as blending of pre-sensitized emulsions (Emulsion E). Use of a single emulsion containing the same dopants as two blended emulsions, produce about the same SPEED but sharper TOE and slightly higher INmax (Emulsion C). It is also evident from Table I and Table II that the sensitization of blended emulsions (Emulsion D) or blending of sensitized emulsions (Emulsion E) result in a significant improvement of the optical and laser LIK instability over a single emulsion containing the same "total" amount of dopants (Emulsion C). The slightly lower INmax values obtained for Emulsions D and E relative to Emulsion C can be overcome by using a bit higher emulsion silver laydown, while maintaining the significant LIK instability improvement.

## EXAMPLE 2

[0076] This example compares effects of blending of emulsion doped with Formula (I) dopant  $K_4Ru(CN)_6$  with emulsion doped with Formula (II) dopant  $Cs_2(II)Os[NO]Cl_5$  on optical and laser Latent Image Keeping (LIK). In each case, silver chloride cubic emulsions sensitized for green color record were used. The sensitization details are as follows:

**Emulsion M:** A portion of silver chloride Emulsion EM-1 was optimally sensitized by the addition Spectral Sensitizing Dye B, followed by addition of optimum amount of gold sulfide. The emulsion was then heated to 60°C and held at this temperature for 33 minutes with subsequent addition Lippmann bromide, followed by addition of 1-(3-acetamidophenyl)-5-mercaptopotrazole. Then the emulsion was cooled to 40°C. The thus obtained silver chloride emulsion was designated as emulsion M.

**Emulsion N:** A portion of silver chloride Emulsion EM-2 was sensitized exactly as in the procedure for the preparation of emulsion M. The thus obtained silver chloride emulsion was designated as emulsion N.

**Emulsion O:** A portion of silver chloride Emulsion EM-3 was sensitized exactly as in the procedure for the preparation of emulsion M. The thus obtained silver chloride emulsion was designated as emulsion O.

**Emulsion P:** A equal portion of silver chloride Emulsion EM-1 and EM-2 was blended and then sensitized exactly as in the procedure for the preparation of emulsion M. The thus obtained silver chloride emulsion was designated as emulsion P. The "total" amounts of each dopant per Ag mole are the same as in Emulsion O.

**Emulsion R:** A equal portion of silver chloride Emulsion M and N was blended. The thus obtained silver chloride emulsion was designated as emulsion R. The "total" amounts of each dopant per Ag mole are the same as in Emulsion O.

Sensitometric data is summarized in Table III and IV.

Table III.

Optical Sensitometry and Optical LIK Data.								
Emulsion	Dmin	SPEED	TOE	INmax	Optical LIK			
					5 min to 2 hr		5 min to 24 hr	
					$\Delta D$ at SPEED	$\Delta D$ at SPEED+ 0.3logE	$\Delta D$ at SPEED	$\Delta D$ at SPEED+ 0.3logE
M	0.111	164	0.415	2.146	0.0776	0.1998	0.1110	0.2194
N	0.117	119	0.352	2.314	0.0501	0.0778	0.0898	0.1296
O	0.111	148	0.413	2.386	0.1556	0.3329	0.1998	0.4012
P	0.110	148	0.474	2.361	0.0722	0.1501	0.0942	0.1995
R	0.096	149	0.471	2.349	0.0278	0.0722	0.0611	0.1002

Table IV

Laser Sensitometry and Laser LIK Data.									
Emulsion	Dmin	SPEED	TOE	INmax	Laser LIK				
					20 sec to 2 min		20 sec to 2 hr		20 sec to 24 hr
					$\Delta D$ at SPEED	$\Delta D$ at SPEED + 0.3logE	$\Delta D$ at SPEED	$\Delta D$ at SPEED + 0.3logE	
M	0.116	114	0.439	2.082	0.0857	0.2276	0.0904	0.2416	0.2665
N	0.114	70	0.375	2.282	0.0514	0.1112	0.0571	0.1144	0.1428
O	0.113	98	0.430	2.312	0.1089	0.3238	0.1143	0.3619	0.4012
P	0.112	98	0.493	2.298	0.0191	0.0476	0.0414	0.1211	0.1422
R	0.111	99	0.491	2.293	0.0238	0.0571	0.0762	0.1714	0.2001

[0077] It is clear from the Table III and IV, that sensitization of a blended emulsion (Emulsion P) produce about the same photographic response as blending of pre-sensitized emulsions (Emulsion R). Use of a single emulsion containing the same dopants as two blended emulsions, produce about the SPEED but sharper TOE and slightly higher INmax (Emulsion O). It is also evident from Table III and Table IV that the sensitization of blended emulsions (Emulsion P) or blending of sensitized emulsions (Emulsion R) result in a significant improvement of the optical and laser LIK instability over a single emulsion containing the same "total" amount of dopants (Emulsion O). The slightly lower INmax values obtained for Emulsions P and R relative to Emulsion O can be overcome by using a bit higher emulsion silver laydown, while maintaining the significant LIK instability improvement.

### EXAMPLE 3

[0078] This example compares effects of blending of emulsion doped with Formula (I) dopant  $K_4Ru(CN)_6$  with emulsion doped with Formula (II) dopant  $Cs_2(II)Os[NO]Cl_5$  on optical and laser Latent Image Keeping (LIK). In each case, silver chloride cubic emulsions sensitized for blue color record were used. The sensitization details are as follows:

Emulsion S: A portion of silver chloride Emulsion EM-1 was optimally sensitized by the addition of p-glutaramido-phenyl disulfide, followed by addition of optimum amount of gold sulfide. The emulsion was then heated to 60°C and held at this temperature for 18 minutes with subsequent addition of Spectral Sensitizing Dye C, followed by Lippmann bromide, followed by addition of 1-(3-acetamidophenyl)-5-mercaptotetrazole. Then the emulsion was cooled to 40°C. The thus obtained silver chloride emulsion was designated as emulsion S.

Emulsion T: A portion of silver chloride Emulsion EM-2 was sensitized exactly as in the procedure for the preparation of emulsion S. The thus obtained silver chloride emulsion was designated as emulsion T.

Emulsion U: A portion of silver chloride Emulsion EM-3 was sensitized exactly as in the procedure for the preparation of emulsion S. The thus obtained silver chloride emulsion was designated as emulsion U.

Emulsion W: An equal portion of silver chloride Emulsion EM-1 and EM-2 was blended and then sensitized exactly as in the procedure for the preparation of emulsion S. The thus obtained silver chloride emulsion was designated as emulsion W. The "total" amounts of each dopant per Ag mole are the same as in Emulsion U.

Emulsion Z: An equal portion of silver chloride Emulsion S and T was blended. The thus obtained silver chloride emulsion was designated as emulsion Z. The "total" amounts of each dopant per Ag mole are the same as in Emulsion U.

Sensitometric data is summarized in Table V and VI.

Table V.

Optical Sensitometry and Optical LIK Data.								
Emulsion	Dmin	SPEED	TOE	INmax	Optical LIK			
					5 min to 2 hr		5 min to 24 hr	
					$\Delta D$ at SPEED	$\Delta D$ at SPEED+ 0.3logE	$\Delta D$ at SPEED	$\Delta D$ at SPEED+ 0.3logE
S	0.085	58	0.306	2.458	0.0409	0.0707	0.0541	0.0878
T	0.095	74	0.342	2.361	0.0219	0.0302	0.0241	0.0414
U	0.096	62	0.326	2.488	0.0708	0.1512	0.0978	0.1806
W	0.098	69	0.365	2.452	0.0302	0.0556	0.0307	0.0609
Z	0.092	68	0.356	2.43	0.0273	0.0487	0.0409	0.0643

Table VI

Laser Sensitometry and Laser LIK Data.								
Emulsion	Dmin	SPEED	TOE	INmax	Laser LIK			
					2min to 2 hr		2 min to 24 hr	
					$\Delta D$ at SPEED	$\Delta D$ at SPEED+ 0.3logE	$\Delta D$ at SPEED	$\Delta D$ at SPEED+ 0.3logE
S	0.067	135	0.312	2.397	0.0551	0.0881	0.0660	0.1155
T	0.081	151	0.355	2.277	0.0340	0.0581	0.0395	0.0690
U	0.062	145	0.326	2.423	0.1001	0.2037	0.1245	0.2367
W	0.078	146	0.354	2.412	0.0441	0.0671	0.0551	0.0781
Z	0.071	144	0.346	2.409	0.0275	0.0606	0.0385	0.0771

[0079] It is clear from the Table V and VI, that sensitization of a blended emulsion (Emulsion W) produce about the same photographic response as blending of pre-sensitized emulsions (Emulsion Z). Use of a single emulsion containing the same dopants as two blended emulsions, produce about the same SPEED but sharper TOE and slightly higher INmax (Emulsion U). It is also evident from Table V and Table VI that the sensitization of blended emulsions (Emulsion W) or blending of sensitized emulsions (Emulsion Z) result in a significant improvement of the optical and laser LIK instability over a single emulsion containing the same "total" amount of dopants (Emulsion U). The slightly lower INmax values obtained for Emulsions W and Z relative to Emulsion U can be overcome by using a bit higher emulsion silver laydown, while maintaining the significant LIK instability improvement.

[0080] It is specifically contemplated that emulsions in accordance with the invention may be sensitized with red, green, and blue sensitizing dyes and be incorporated in a color paper format as described in Example 4 of U.S. Patent 5,783,373.

### Claims

1. A photographic element comprising a support bearing at least one radiation-sensitive silver halide emulsion layer comprising silver halide grains containing greater than 50 mole percent chloride, based on silver, and having greater than 50 percent of their surface area provided by {100} crystal faces, wherein

(i) a first fraction which comprises from 10-90 wt% of the silver halide grains, based on total radiation-sensitive silver halide in the layer, consists of grains which have a central portion accounting for up to 99 percent of total silver which contains at least  $10^{-7}$  mole of a hexacoordination metal complex which satisfies formula (I) per mole of silver and less than  $10^{-10}$  mole of a hexacoordination metal complex which satisfies formula (II) per mole of silver, and

(ii) a second fraction which comprises from 10-90 wt% of the silver halide grains, based on total radiation-sensitive silver halide in the layer, consists of grains which have a central portion accounting for up to 99 percent of total silver which contains at least  $10^{-10}$  mole of a hexacoordination metal complex which satisfies the formula (II) per mole of silver and less than  $10^{-7}$  mole of a hexacoordination metal complex which satisfies the formula (I) per mole of silver:



wherein n is zero, -1, -2, -3 or -4,

M is a filled frontier orbital polyvalent metal ion, other than iridium, and

$L_6$  represents bridging ligands which can be independently selected, provided that at least four of the ligands are anionic ligands, and at least one of the ligands is a cyano ligand or a ligand more electronegative than a cyano ligand;



where T is a Os or Ru;

$E_4$  represents bridging ligands which can be independently selected;

$E'$  is E or NZ;

$r$  is zero, -1, -2 or -3; and

Z is oxygen or sulfur.

2. An element according to claim 1 wherein the first and second fractions of the silver halide grains each comprise from 25-75 wt% of the total radiation-sensitive silver halide in the emulsion layer.
3. An element according to claim 2 wherein the first and second fractions of the silver halide grains each comprise from 40-60 wt% of the total radiation-sensitive silver halide in the emulsion layer.
4. An element according to any one of claims 1-3 wherein in the first fraction of silver halide grains the dopant of Formula (I) is located within the central portion of grains in a concentration of from  $10^{-8}$  to  $10^{-3}$  mole per mole of silver, and in the second fraction of silver halide grains the dopant of Formula (II) is located within the central portion of the grains in a concentration of from  $10^{-10}$  to  $10^{-7}$  mole per mole of silver.
5. An element according to claim 4 wherein the first fraction of silver halide grains contains from  $10^{-6}$  to  $10^{-4}$  mole of a hexacoordination metal complex of Formula (I) per mole of silver.
6. An element according to claim 4 or 5 wherein the second fraction of silver halide grains contains from  $10^{-9}$  to  $10^{-8}$  mole of a hexacoordination metal complex of Formula (II) per mole of silver.
7. An element according to any one of claims 1-6 wherein M represents an iron, ruthenium or osmium ion.
8. An element according to any one of claims 1-7 wherein each of the bridging ligands of the dopant of Formula (I) are at least as electronegative as cyano ligands.
9. An element according to claim 8 wherein the dopant of Formula (I) is  $[Ru(CN)_6]^{-4}$  and the dopant of Formula (II) is  $[Os(NO)Cl_5]^{-2}$ .
10. An electronic printing method which comprises subjecting the radiation sensitive silver halide emulsion layer of a recording element according to any one of claims 1-9 to actinic radiation of at least  $10^{-4}$  ergs/cm<sup>2</sup> for up to 100  $\mu$  seconds duration in a pixel-by-pixel mode.



European Patent  
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## EUROPEAN SEARCH REPORT

Application Number  
EP 02 07 7966

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
A	US 6 033 831 A (IKEDA TSUYOSHI ET AL) 7 March 2000 (2000-03-07) * column 5, line 36 - column 6, line 68 * * column 7, line 59 - line 68 * * claim 7; tables 6-8 *	1-10	G03C1/09
D,A	US 5 597 686 A (MACINTYRE GLADYS L ET AL) 28 January 1997 (1997-01-28) * claims 1-10 *	1-10	
D,A	US 5 783 373 A (BELL ERIC L ET AL) 21 July 1998 (1998-07-21) * claim 1 *	1-10	
A	EP 0 718 676 A (EASTMAN KODAK CO) 26 June 1996 (1996-06-26) * page 8, line 18 - page 9, line 5 * * page 10, line 9 - line 38; claim 1 *	1-10	
A	US 5 418 118 A (EDWARDS JAMES L ET AL) 23 May 1995 (1995-05-23) * column 55, line 34 - line 52; claims 23,28 *	1-10	
			TECHNICAL FIELDS SEARCHED (Int.Cl.7)
			G03C
The present search report has been drawn up for all claims			
Place of search <b>THE HAGUE</b>		Date of completion of the search <b>21 November 2002</b>	Examiner <b>Bolger, W</b>
CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons A : member of the same patent family, corresponding document	
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**ANNEX TO THE EUROPEAN SEARCH REPORT  
ON EUROPEAN PATENT APPLICATION NO.**

EP 02 07 7966

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on  
The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

21-11-2002

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 6033831 A	07-03-2000	JP 11305349 A	05-11-1999
		EP 0952484 A2	27-10-1999
US 5597686 A	28-01-1997	DE 69406562 D1	11-12-1997
		DE 69406562 T2	04-06-1998
		EP 0610670 A1	17-08-1994
		JP 6242539 A	02-09-1994
US 5783373 A	21-07-1998	NONE	
EP 0718676 A	26-06-1996	EP 0718676 A1	26-06-1996
		JP 8234340 A	13-09-1996
		US 5728516 A	17-03-1998
US 5418118 A	23-05-1995	DE 69528093 D1	17-10-2002
		EP 0668535 A2	23-08-1995
		FR 2716546 A1	25-08-1995
		JP 8036247 A	06-02-1996
		US 5512103 A	30-04-1996

EPC FORM P446

For more details about this annex : see Official Journal of the European Patent Office, No. 12/82